

54. For four heads: $W = 1 \rightarrow \Delta S = k \ln W = (1.38 \times 10^{-23} \text{ J/K}) \ln 1 = \boxed{0}$
 For 3 heads, 1 tail: $W = 4 \rightarrow \Delta S = k \ln W = (1.38 \times 10^{-23} \text{ J/K}) \ln 4 = \boxed{1.91 \times 10^{-23} \text{ J/K}}$
 For 2 heads, 2 tails: $W = 6 \rightarrow \Delta S = k \ln W = (1.38 \times 10^{-23} \text{ J/K}) \ln 6 = \boxed{2.47 \times 10^{-23} \text{ J/K}}$
 For 1 head, 3 tails: $W = 4 \rightarrow \Delta S = k \ln W = (1.38 \times 10^{-23} \text{ J/K}) \ln 4 = \boxed{1.91 \times 10^{-23} \text{ J/K}}$
 For four tails: $W = 1 \rightarrow \Delta S = k \ln W = (1.38 \times 10^{-23} \text{ J/K}) \ln 1 = \boxed{0}$

55. From the table below, we see that there are a total of $2^6 = 64$ microstates.

Macrostate	Possible Microstates (H = heads, T = tails)						Number of Microstates
6 heads, 0 tails	H H H H H H						1
5 heads, 1 tails	H H H H H T						6
4 heads, 2 tails	H H H H T T						15
	H H H T H T						
3 heads, 3 tails	H H H T T T						20
	H H T H T T						
	H T H T H T						
2 heads, 4 tails	T T T T H H						15
	T T T H T T						
1 heads, 5 tails	T T T T T H						6
0 heads, 6 tails	T T T T T T						1

- (a) The probability of obtaining three heads and three tails is $\boxed{20/64}$ or $\boxed{5/16}$.
 (b) The probability of obtaining six heads is $\boxed{1/64}$.
56. When throwing two dice, there are 36 possible microstates.
 (a) The possible microstates that give a total of 7 are: (1)(6), (2)(5), (3)(4), (4)(3), (5)(2), and (6)(1). Thus the probability of getting a 7 is $6/36 = \boxed{1/6}$.
 (b) The possible microstates that give a total of 11 are: (5)(6) and (6)(5). Thus the probability of getting an 11 is $2/36 = \boxed{1/18}$.
 (c) The possible microstates that give a total of 4 are: (1)(3), (2)(2), and (3)(1). Thus the probability of getting a 4 is $3/36 = \boxed{1/12}$.
57. (a) There is only one microstate for 4 tails: TTTT. There are 6 microstates with 2 heads and 2 tails: HHTT, HTHT, HTTH, THHT, THTH, and TTHH. Use Eq. 20-14 to calculate the entropy change.

$$\Delta S = k \ln W_2 - k \ln W_1 = k \ln \frac{W_2}{W_1} = (1.38 \times 10^{-23} \text{ J/K}) \ln 6 = \boxed{2.47 \times 10^{-23} \text{ J/K}}$$

(b) Apply Eq. 20-14 again. There is only 1 final microstate, and about 1.0×10^{29} initial microstates.

$$\Delta S = k \ln W_2 - k \ln W_1 = k \ln \frac{W_2}{W_1} = (1.38 \times 10^{-23} \text{ J/K}) \ln \left(\frac{1}{1.0 \times 10^{29}} \right) = \boxed{-9.2 \times 10^{-22} \text{ J/K}}$$

(c) These changes are much smaller than those for ordinary thermodynamic entropy changes.

For ordinary processes, there are many orders of magnitude more particles than we have considered in this problem. That leads to many more microstates and larger entropy values.

58. The number of microstates for macrostate A is $W_A = \frac{10!}{10!0!} = 1$. The number of microstates for

macrostate B is $W_B = \frac{10!}{5!5!} = 252$.

$$(a) \Delta S = k \ln W_B - k \ln W_A = k \ln \frac{W_B}{W_A} = (1.38 \times 10^{-23} \text{ J/K}) \ln 252 = \boxed{7.63 \times 10^{-23} \text{ J/K}}$$

Since $\Delta S > 0$, this can occur naturally.

$$(b) \Delta S = k \ln W_A - k \ln W_B = -k \ln \frac{W_B}{W_A} = -(1.38 \times 10^{-23} \text{ J/K}) \ln 252 = \boxed{-7.63 \times 10^{-23} \text{ J/K}}$$

Since $\Delta S < 0$, this cannot occur naturally.

60. The required area is $\left(22 \frac{10^3 \text{ W h}}{\text{day}} \right) \left(\frac{1 \text{ day}}{9 \text{ h Sun}} \right) \left(\frac{1 \text{ m}^2}{40 \text{ W}} \right) = 61 \text{ m}^2 \approx \boxed{60 \text{ m}^2}$. A small house with

1000 ft² of floor space, and a roof tilted at 30°, would have a roof area of

$$\left(1000 \text{ ft}^2 \right) \left(\frac{1}{\cos 30^\circ} \right) \left(\frac{1 \text{ m}}{3.28 \text{ ft}} \right)^2 = 110 \text{ m}^2, \text{ which is about twice the area needed, and so } \boxed{\text{the}}$$

cells would fit on the house. But not all parts of the roof would have 9 hours of sunlight, so more than the minimum number of cells would be needed.

77. We need to find the efficiency in terms of the given parameters, T_H , T_L , V_a , and V_b . So we must find the net work done and the heat input to the system. The work done during an isothermal process is given by Eq. 19-8. The work done during an isovolumetric process is 0. We also use the first law of thermodynamics.

$$\text{ab (isothermal):} \quad \Delta E_{\text{int}} = 0 = Q_{\text{ab}} - W_{\text{ab}} \rightarrow Q_{\text{ab}} = W_{\text{ab}} = nRT_H \ln \frac{V_b}{V_a} > 0$$

bc (isovolumetric):

$$\Delta E_{\text{int}} = Q_{\text{bc}} - 0 \rightarrow Q_{\text{bc}} = \Delta E_{\text{int}} = nC_V (T_L - T_H) = \frac{3}{2} nR (T_L - T_H) < 0$$

cd (isothermal):

$$\Delta E_{\text{int}} = 0 = Q_{\text{cd}} - W_{\text{cd}} \rightarrow Q_{\text{cd}} = W_{\text{cd}} = nRT_L \ln \frac{V_a}{V_b} = -nRT_L \ln \frac{V_b}{V_a} < 0$$

da (isovolumetric):

$$\Delta E_{\text{int}} = Q_{\text{da}} - 0 \rightarrow Q_{\text{da}} = \Delta E_{\text{int}} = nC_V (T_H - T_L) = \frac{3}{2} nR (T_H - T_L) > 0$$

$$W = W_{\text{ab}} + W_{\text{cd}} = nRT_H \ln \frac{V_b}{V_a} - nRT_L \ln \frac{V_b}{V_a} = nR (T_H - T_L) \ln \frac{V_b}{V_a}$$

$$Q_{\text{in}} = Q_{\text{ab}} + Q_{\text{da}} = nRT_H \ln \frac{V_b}{V_a} + \frac{3}{2} nR (T_H - T_L)$$

$$e_{\text{Sterling}} = \frac{W}{Q_{\text{in}}} = \frac{(T_H - T_L) \ln \frac{V_b}{V_a}}{T_H \ln \frac{V_b}{V_a} + \frac{3}{2} (T_H - T_L)} = \left(\frac{T_H - T_L}{T_H} \right) \left[\frac{\ln \frac{V_b}{V_a}}{\ln \frac{V_b}{V_a} + \frac{3}{2} \left(\frac{T_H - T_L}{T_H} \right)} \right]$$

$$= e_{\text{Carnot}} \left[\frac{\ln \frac{V_b}{V_a}}{\ln \frac{V_b}{V_a} + \frac{3}{2} \left(\frac{T_H - T_L}{T_H} \right)} \right]$$

Since the factor in [] above is less than 1, we see that $e_{\text{Sterling}} < e_{\text{Carnot}}$.