

**PHYSICS 110A : CLASSICAL MECHANICS  
DISCUSSION #2 PROBLEMS**

[1] Solve the equation

$$L_t x \equiv \ddot{x} + (a + b + c) \dot{x} + (ab + ac + bc) x + abc x = f_0 \cos(\Omega t) . \quad (1)$$

*Solution* – The key to solving this was the hint that the differential operator  $L_t$  could be written as

$$\begin{aligned} L_t &= \frac{d^3}{dt^3} + (a + b + c) \frac{d^2}{dt^2} + (ab + ac + bc) \frac{d}{dt} + abc \\ &= \left( \frac{d}{dt} + a \right) \left( \frac{d}{dt} + b \right) \left( \frac{d}{dt} + c \right) , \end{aligned} \quad (2)$$

which says that the third order differential operator appearing in the ODE is in fact a product of first order differential operators. Since

$$\frac{dx}{dt} + \alpha x = 0 \implies x(t) = A e^{-\alpha t} , \quad (3)$$

we see that the homogeneous solution takes the form

$$x_h(t) = A e^{-at} + B e^{-bt} + C e^{-ct} , \quad (4)$$

where  $A$ ,  $B$ , and  $C$  are constants.

To find the inhomogeneous solution, we solve  $L_t x = f_0 e^{-i\Omega t}$  and take the real part. Writing  $x(t) = x_0 e^{-i\Omega t}$ , we have

$$L_t x_0 e^{-i\Omega t} = (a - i\Omega)(b - i\Omega)(c - i\Omega) x_0 e^{-i\Omega t} \quad (5)$$

and thus

$$x_0 = \frac{f_0 e^{-i\Omega t}}{(a - i\Omega)(b - i\Omega)(c - i\Omega)} \equiv A(\Omega) e^{i\delta} f_0 e^{-i\Omega t} ,$$

where

$$A(\Omega) = \left[ (a^2 + \Omega^2)(b^2 + \Omega^2)(c^2 + \Omega^2) \right]^{-1/2} \quad (6)$$

$$\delta(\Omega) = \tan^{-1} \left( \frac{\Omega}{a} \right) + \tan^{-1} \left( \frac{\Omega}{b} \right) + \tan^{-1} \left( \frac{\Omega}{c} \right) . \quad (7)$$

Thus, the most general solution to  $L_t x(t) = f_0 \cos(\Omega t)$  is

$$x(t) = A(\Omega) f_0 \cos(\Omega t - \delta(\Omega)) + A e^{-at} + B e^{-bt} + C e^{-ct} . \quad (8)$$

Note that the phase shift increases monotonically from  $\delta(0) = 0$  to  $\delta(\infty) = \frac{3}{2}\pi$ .

[2] Consider the potential

$$U(x) = U_0 (x^2 - a^2) (x^2 - 4a^2) (x^2 - 9a^2) . \quad (9)$$

Sketch  $U(x)$  and the phase curves.

*Solution* – Clearly  $U(x \rightarrow \pm\infty) = \infty$ , and  $U(x)$  has zeros at  $x = \pm a$ ,  $x = \pm 2a$ , and  $x = \pm 3a$ . Setting  $U'(x) = 0$  we obtain  $x = 0$  and also a quadratic equation in  $x^2$ , with roots at  $x^2 = 7a^2$  and  $x^2 = \frac{7}{3}a^2$ . Plugging in, we find the three local minima, at  $x = \pm\sqrt{7} a$  and  $x = 0$  are all degenerate, with  $U = -36U_0 a^6$ , and the two maxima at  $x = \pm\sqrt{\frac{7}{3}} a$  have  $U = \frac{400}{27} U_0 a^6$ . This is a nice problem for Ben Schmidel's phase plotter.

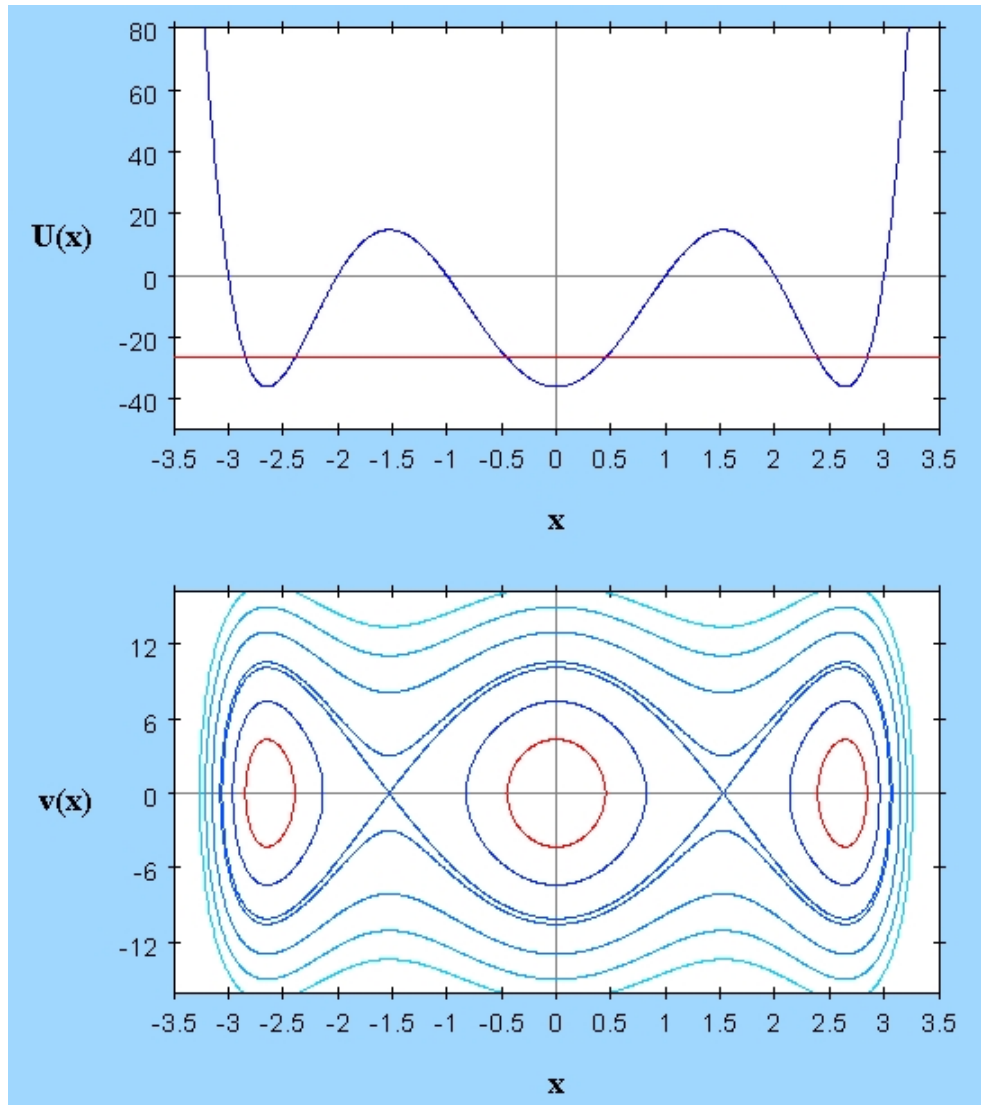


Figure 1:  $U(x) = (x^2 - 1) (x^2 - 4) (x^2 - 9)$  and associated phase curves.

[3] Consider the van der Pol oscillator,

$$\ddot{x} + 2\mu(x^2 - 1)\dot{x} + x = 0 . \quad (10)$$

Find and classify the fixed point(s), find the nullclines, sketch the phase flow, and argue that a stable limit cycle exists.

*Solution* – With  $v = \dot{x}$ , we have

$$\dot{x} = v \quad , \quad \dot{v} = -x + \mu(1 - x^2)v . \quad (11)$$

Since both  $\dot{x} = 0$  and  $\dot{v} = 0$  at a fixed point, we find a unique fixed point at  $(x, v) = (0, 0)$ . Linearizing about the fixed point, we write  $x = 0 + \delta x$ ,  $v = 0 + \delta v$ , with

$$\frac{d}{dt} \begin{pmatrix} \delta x \\ \delta v \end{pmatrix} = \overbrace{\begin{pmatrix} 0 & 1 \\ -1 & \mu \end{pmatrix}}^M \begin{pmatrix} \delta x \\ \delta v \end{pmatrix} . \quad (12)$$

The matrix  $M$  has trace  $T = \mu$  and determinant  $D = +1$ . Thus, according to the fixed point classification scheme derived in class and in the notes, the fixed point  $(0, 0)$  is a stable node if  $\mu > 2$  and a stable spiral if  $\mu < 2$ .

The nullclines are curves along which  $\dot{x} = 0$  or  $\dot{v} = 0$ . The equation of the  $x$  nullcline is  $v = 0$ , *i.e.* the  $x$ -axis. Along the  $x$ -axis, then, the flow must be purely up or down, with no

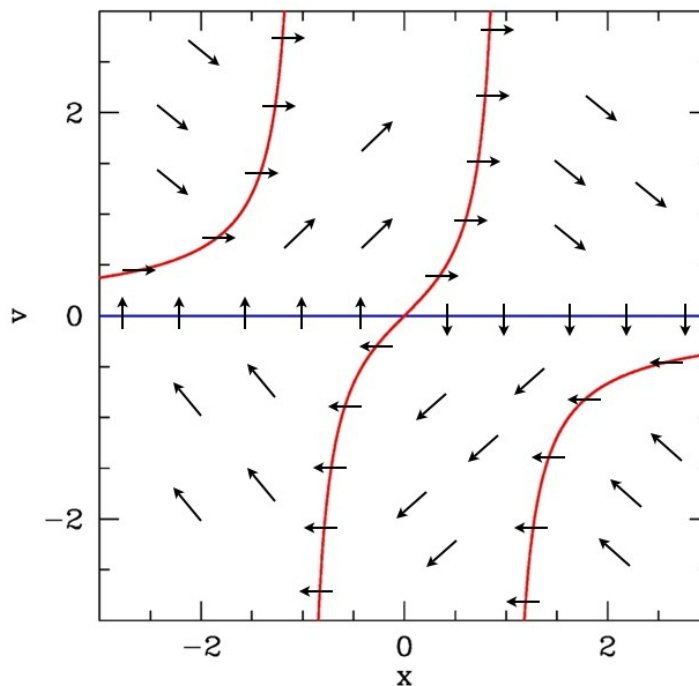


Figure 2: Sketch of phase flow for the van der Pol system. Only the general direction of the flow is shown. Blue line:  $x$  nullcline; red line:  $v$  nullcline.

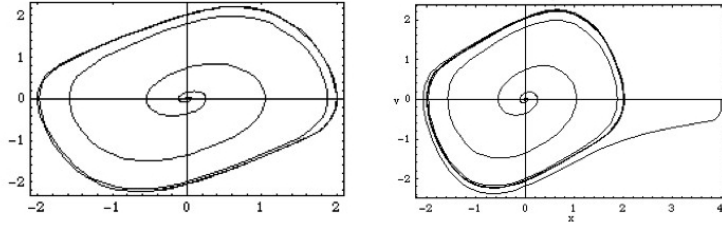


Figure 3: Evolution of the van der Pol equation for  $\mu = \frac{1}{2}$ , starting from two initial conditions. The flow spirals toward the stable limit cycle.

$x$  component. The equation of the  $v$  nullcline is

$$v = \frac{1}{\mu} \frac{x}{1 - x^2} . \quad (13)$$

The nullclines and the flow are sketched in Fig. 2. Note that the  $x$ -component of the phase velocity  $\dot{\varphi}$  changes sign across an  $x$ -nullcline, and the  $v$ -component of  $\dot{\varphi}$  changes sign across a  $v$ -nullcline.

The limit cycle is shown in Figs. 3 and 4.

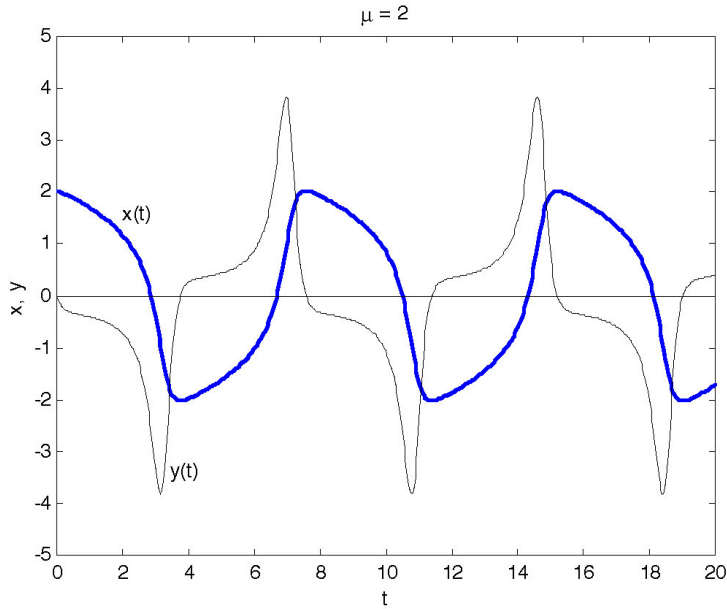


Figure 4:  $x(t)$  and  $v(t)$  ( $y(t)$  in this plot) for the van der Pol system, with  $\mu = 2$ .

[4] Consider the following circuit and construct a mechanical analog.

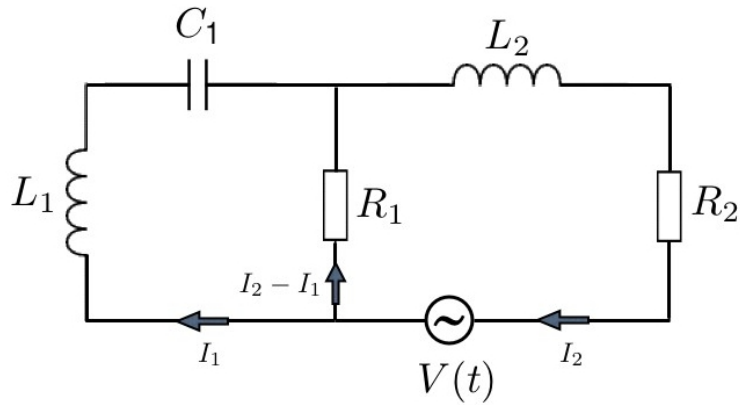


Figure 5: A driven  $L$ - $C$ - $R$  circuit, with  $V(t) = V_0 \cos(\omega t)$ .

*Solution* – We invoke Kirchoff’s laws around the left and right loops:

$$L_1 \dot{I}_1 + \frac{Q_1}{C_1} + R_1 (I_1 - I_2) = 0 \quad (14)$$

$$L_2 \dot{I}_2 + R_2 I_2 + R_1 (I_2 - I_1) = V(t) . \quad (15)$$

Let  $Q_1(t)$  be the charge on the left plate of capacitor  $C_1$ , and define

$$Q_2(t) = \int_0^t dt' I_2(t') . \quad (16)$$

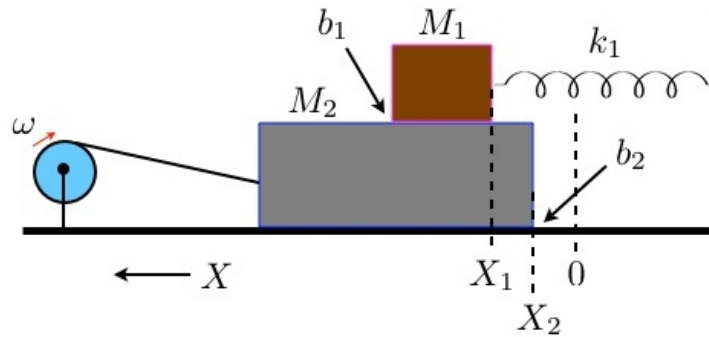


Figure 6: The equivalent mechanical circuit.

Then Kirchoff's laws may be written

$$\ddot{Q}_1 + \frac{R_1}{L_1} (\dot{Q}_1 - \dot{Q}_2) + \frac{1}{L_1 C_1} Q_1 = 0 \quad (17)$$

$$\ddot{Q}_2 + \frac{R_2}{L_2} \dot{Q}_2 + \frac{R_1}{L_2} (\dot{Q}_2 - \dot{Q}_1) = \frac{V(t)}{L_2} . \quad (18)$$

Now consider the mechanical system in Fig. 6. The blocks have masses  $M_1$  and  $M_2$ . The friction coefficient between blocks 1 and 2 is  $b_1$ , and the friction coefficient between block 2 and the floor is  $b_2$ . There is a spring of spring constant  $k_1$  which connects block 1 to the wall. Finally, block 2 is driven by a periodic acceleration  $f_0 \cos(\omega t)$ . We now identify

$$X_1 \leftrightarrow Q_1 \quad , \quad X_2 \leftrightarrow Q_2 \quad , \quad b_1 \leftrightarrow \frac{R_1}{L_1} \quad , \quad b_2 \leftrightarrow \frac{R_2}{L_2} \quad , \quad k_1 \leftrightarrow \frac{1}{L_1 C_1} \quad , \quad (19)$$

as well as  $f(t) \leftrightarrow V(t)/L_2$ .