

# Lecture 12

1.

## Introduction to Fluid Mechanics II.

### Momentum flux

$$\frac{\partial}{\partial t} (\rho v_i) = \rho \frac{\partial v_i}{\partial t} + \frac{\partial \rho}{\partial t} v_i$$

rate of change  
in momentum  
components  
 $i = 1, 2, 3$

continuity eq.  $\frac{\partial \rho}{\partial t} = - \frac{\partial (\rho v_k)}{\partial x_k}$

fixed unit volume!

Euler eq.  $\frac{\partial v_i}{\partial t} = - v_k \frac{\partial v_i}{\partial x_k} - \frac{1}{\rho} \frac{\partial p}{\partial x_i}$

$$\begin{aligned} \frac{\partial}{\partial t} (\rho v_i) &= - \rho v_k \frac{\partial v_i}{\partial x_k} - \frac{\partial p}{\partial x_i} - v_i \frac{\partial (\rho v_k)}{\partial x_k} \\ &= - \frac{\partial p}{\partial x_i} - \frac{\partial}{\partial x_k} (\rho v_i v_k) \end{aligned}$$

write  $\frac{\partial p}{\partial x_i} = \delta_{ik} \frac{\partial p}{\partial x_k}$

summation over  
repeated indices

$$\frac{\partial}{\partial t} (\rho v_i) = - \frac{\partial \Pi_{ik}}{\partial x_k}$$

rate of change in  
momentum

$$\Pi_{ik} = p \delta_{ik} + \rho v_i v_k$$

What is the meaning of  $\Pi_{ik}$ ?

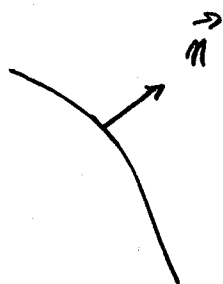
2.

$$\frac{d}{dt} \int \rho v_i dV = - \int \frac{\partial \Pi_{ik}}{\partial x_k} dV$$

rate of change of  
momentum ( $i$ th component)  
in fixed volume

$$= - \oint \Pi_{ik} df_k$$

momentum flowing out  
through bounding surface  
of volume



$$df_k = n_k \cdot df$$

area of surface element

$\Pi_{ik} \cdot n_k$  flux of  $i$ th momentum component through  
unit surface area

$$\Pi_{ik} n_k = p \cdot n_i + \int \rho v_i v_k \cdot n_k$$

$p \cdot \vec{n} + \int \rho \vec{v} (\vec{v} \cdot \vec{n})$  in vector form  
momentum flux in  
direction of  $\vec{n}$

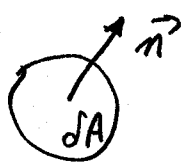
$\Pi_{ik}$  momentum flux density tensor

$i$ th component of the amount of momentum  
flowing in unit time through unit area  
perpendicular to the  $x_k$ -axis

## Stress tensor

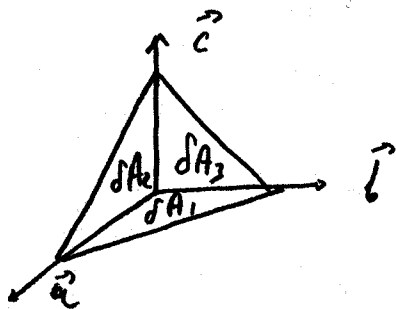
If an element of mass of fluid is acted on by short-range forces arising from interaction with fluid molecules outside this element, these short range forces can act only on a thin layer

$$\vec{\Sigma}(\vec{n}, \vec{x}, t) \, dA \quad \begin{array}{l} \text{force exerted on surface} \\ \text{element} \\ \text{surface area} \end{array}$$



$\vec{\Sigma}$  is stress exerted by the fluid on the side of the surface element to which  $\vec{n}$  points, on the fluid on the side which  $\vec{n}$  points away from

$$\begin{aligned} & - \vec{\Sigma}(\vec{n}, \vec{x}, t) \, dA \quad \text{force exerted across the surface} \\ & = \vec{\Sigma}(-\vec{n}, \vec{x}, t) \, dA \quad \text{element on the fluid on the side} \\ & \quad \text{to which } \vec{n} \text{ points} \end{aligned}$$



tetrahedron volume element

$$\vec{\Sigma}(\vec{n}) \, dA + \vec{\Sigma}(-\vec{a}) \, dA_1 + \vec{\Sigma}(-\vec{b}) \, dA_2 + \vec{\Sigma}(-\vec{c}) \, dA_3$$

total force on volume element  $\vec{x}$  dependence negligible

$$\delta A_1 = \vec{a} \cdot \vec{n} \delta A$$

$$\delta A_2 = \vec{b} \cdot \vec{n} \delta A$$

$$\delta A_3 = \vec{c} \cdot \vec{n} \delta A$$

$$\left[ \Sigma_i (n) - \left\{ a_j \Sigma_i (\vec{a}) + b_j \Sigma_i (\vec{b}) + c_j \Sigma_i (\vec{c}) \right\} n_j \right] \delta A$$

$i^{\text{th}}$  component of total force

$\delta V$  much smaller than  $\delta A$  in  $\delta V \rightarrow 0$  limit

mass  $\times$  acceleration in tetrahedron is  $\sim \delta V$

= resultant of body forces  $\sim \delta V$  + resultant of surface forces  $\sim \delta A$



$$\Sigma_i (n) = \left\{ a_j \Sigma_i (\vec{a}) + b_j \Sigma_i (\vec{b}) + c_j \Sigma_i (\vec{c}) \right\} n_j$$

$\vec{n}, \vec{\Sigma}$  do not depend on choice of reference axes  $\Rightarrow \{ \}_{ij}$  must be represented

by reference independent tensor

$$\Sigma_i (n) = \sigma_{ij} n_j$$

$\sigma_{ij}$  stress tensor

It is the  $i$ th component of the force per unit area exerted across a plane surface element normal to the  $j$ -direction, at position  $\vec{x}$  in the fluid and at time  $t$

$\sigma_{ij} = \sigma_{ji}$  six independent components

symmetric

3 diagonal normal stresses

non-diagonal tangential stresses

$\sigma_{ij} = -p \delta_{ij}$  for fluid at rest

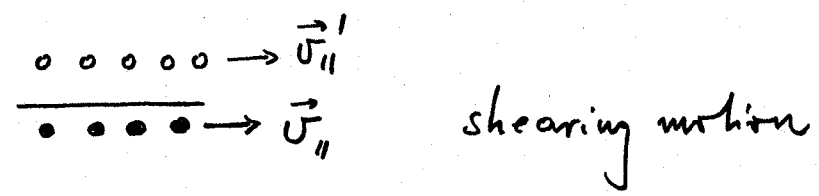
↑ static fluid pressure

For moving fluid the combined effect of momentum flux by passage of molecules across the surface element (momentum transport) and forces exerted between molecules on the two sides is represented by the local stress in the fluid.

If velocity is constant in neighborhood of volume element, stress is normal to surface for all orientations of surface element.

If continuum velocity is not uniform, the tangential components of stress may not be zero.

Consider when fluid velocity has component in surface element and a magnitude which varies only normal to the surface element:



tangential component of stress

sign of stress tries to eliminate velocity difference

Transport of momentum across surface constitutes internal friction, viscous fluid motion

Navier - Stokes Eq.

$$\frac{\partial}{\partial t} (\rho v_i) = - \frac{\partial \Pi_{ik}}{\partial x_k} \quad \text{Euler eq.}$$

$$\Pi_{ik} = p \delta_{ik} + \rho v_i v_k - \sigma_{ik} \quad \leftarrow \text{added term!}$$

$$= \sigma_{ik} + \rho v_i v_k$$

$$\sigma_{ik} = - p \delta_{ik} + \overset{\uparrow}{\sigma'_{ik}}$$

viscous stress tensor

$\sigma'_{ik}$  vanishes for  $\vec{v} = \text{const}$

first order in velocity gradient

$$\sigma'_{ik} = \eta \left( \frac{\partial v_i}{\partial x_k} + \frac{\partial v_k}{\partial x_i} - \frac{2}{3} \delta_{ik} \frac{\partial v_l}{\partial x_l} \right) + \zeta \delta_{ik} \frac{\partial v_l}{\partial x_l}$$

↑  
coefficient of viscosity

↑  
second viscosity

$$\eta > 0, \quad \zeta > 0$$

$\sigma'_{ik}$  vanishes if  $\vec{v} = \vec{\Omega} \times \vec{r}$  for body in uniform rotation

$$\rho \left( \frac{\partial v_i}{\partial t} + v_k \frac{\partial v_i}{\partial x_k} \right) = - \frac{\partial p}{\partial x_i} +$$

$$+ \frac{\partial}{\partial x_k} \left\{ \eta \left( \frac{\partial v_i}{\partial x_k} + \frac{\partial v_k}{\partial x_i} - \frac{2}{3} \delta_{ik} \frac{\partial v_l}{\partial x_l} \right) \right\} + \frac{\partial}{\partial x_i} \left( \zeta \frac{\partial v_l}{\partial x_l} \right)$$

if  $\eta, \zeta$  constant:

$$\rho \left[ \frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \text{grad}) \vec{v} \right] = - \text{grad } p + \eta \Delta \vec{v} + \left( \zeta + \frac{1}{3} \eta \right) \text{grad div } \vec{v}$$

Navier - Stokes Eq.

Simplifies for incompressible fluid

8.

$$\rho = \text{const}$$

$$\frac{\partial \rho}{\partial t} + \rho \operatorname{div} \vec{v} + \vec{v} \cdot \operatorname{grad} \rho = 0$$

$$\operatorname{div} \vec{v} = 0 \quad \text{incompressible}$$

$$\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \operatorname{grad}) \vec{v} = -\frac{1}{\rho} \operatorname{grad} p + \frac{\eta}{\rho} \Delta \vec{v}$$

$$\sigma_{ik} = -p \delta_{ik} + \eta \left( \frac{\partial v_i}{\partial x_k} + \frac{\partial v_k}{\partial x_i} \right)$$

$$\nu = \frac{\eta}{\rho} \quad \text{kinetic viscosity} \quad \eta \quad \text{dynamic viscosity}$$

	$\eta$ (g/cm sec)	$\nu$ (cm <sup>2</sup> /sec)	20° C
Water	0.010	0.010	
Air	0.00018	0.150	
Alcohol	0.018	0.022	
Glycerine	8.5	6.8	
Mercury	0.0156	0.0012	